An unsteady heat problem is formulated and solved for the heater of an anti-icing device for the nonmetallic blades of an aircraft propeller. Equations are derived of value in the design of such anti-icing devices.

Electric anti-icing devices are at present the most widely used means of preventing the icing of aircraft propellers. They are usually of multi-layer construction with the heating element cemented inside. The outer layer is electrically insulating and protects the heater from mechanical damage. A thermally insulating layer separates the heater from the material of the blade and is intended to reduce the heat flux to the blade.

Let us examine the heat flow kinetics associated with the operation of the heater of an anti-icing device on a nonmetallic blade. Part of the heat will be anti-icing protective layer and removing ice, while the rest will go to heating the blade. The temperature distribution over a section of the blade will then be approximately as illustrated in the figure. The distribution shown does not take account of differences in the thermophysical properties of the separate layers of the section examined. To facilitate solution of the heat problem and to simplify the result, it is convenient to regard the blade, including the layer of ice, as isotropic. It will then be unnecessary to take account of the different thermophysical properties, and equivalent values of the thermal conductivity and diffusivity may be introduced in formulating the problem. The equivalent values \( \lambda_e \) and \( \alpha_e \) will be close to the real ones, since they are approximately of the same order for the materials used in constructing anti-icing devices. An exception is the outer protective layer of steel, but its thickness in an anti-icing device is small in comparison with the total thickness of the anti-icing device, and its influence on the equivalent thermophysical properties will accordingly be slight.

In addition to this approximation, it may be assumed that the energy losses due to mass transfer do not depend on the temperature of the icing surface. In fact, the vapor pressure of the water over the ice will be a function of temperature. However, we shall assume that, in practice, the vapor pressure of the water over the ice may be taken as the value at the moment when the ice begins to melt, without any appreciable loss of accuracy in the final result. This corresponds to the value at \(-2\) to \(-4^\circ C\). This assumption simplifies the solution of the heat problem considerably.

We also assume that the local heat flux is one-dimensional and has a direction at right angles to the blade surface.

These approximations enable one to formulate the unsteady heat problem illustrated in the figure as follows:

\[
\frac{\partial t_1(u, F_0)}{\partial F_0} = \frac{\partial^2 t_1(u, F_0)}{\partial u^2} \quad (F_0 > 0, \quad 0 < u < 1),
\]

\[
\frac{\partial t_2(u, F_0)}{\partial F_0} = \frac{\partial^2 t_2(u, F_0)}{\partial u^2} \quad (F_0 > 0, \quad 1 < u < \infty).
\]

The boundary conditions will be

\[
t_1(u, 0) = t_2(u, 0) = t_0,
\]

\[
Bi [t_1(0, F_0) - t_2] + \frac{q_0 \delta}{\lambda_e} \frac{\partial t_1(0, F_0)}{\partial u} = 0;
\]

\[
t_1(1, F_0) = t_2(1, F_0),
\]

\[
-\frac{\partial t_1(1, F_0)}{\partial u} + \frac{\partial t_2(1, F_0)}{\partial u} = \frac{q_0 \delta}{\lambda_e},
\]

\[
\frac{\partial t_2(\infty, F_0)}{\partial u} = 0.
\]
Here

\[ q_0 := \frac{a}{c_p} \cdot 0.628L_{\text{vap}} \frac{e_0 - e_{t_0}}{p_a} \quad (3) \]

Since the difference \( e_0 - e_{t_0} \) is assumed to be constant, \( q_0 \) is not a function of time. The equilibrium temperature \( t_0 \) of the surface exposed to icing may be determined from the nomograms presented in [2]. The equivalent values \( \alpha_e \) and \( \lambda_e \) are calculated from the formulas:

\[ \alpha_e = \frac{\lambda_e}{[c \rho]_e}, \quad [c \rho]_e = c_\rho b_1 + c_1 \rho_1 l_1 + c_2 \rho_2 l_2 + \ldots + c_n \rho_n l_n, \]

\[ \lambda_e = (b_1 + l_1 + l_2 + \ldots + l_n) \left( \frac{b_1}{\lambda b_1} + \frac{l_1}{\lambda_1} + \frac{l_2}{\lambda_2} + \ldots + \frac{l_n}{\lambda_n} \right)^{-1}. \]

Solving (1), we obtain the following relations:

\[ t_1(u, F_0) - t_0 = \frac{q_0}{\alpha_e} V_{F_0} \text{erf}c \frac{1-u}{2 \sqrt{F_0}} - Q_1 - Q_2, \quad (4) \]

\[ t_2(u, F_0) - t_0 = \frac{q_0}{\alpha_e} V_{F_0} \text{erf}c \frac{u-1}{2 \sqrt{F_0}} - Q_1 - Q_2, \quad (5) \]

where

\[ Q_1 = -\frac{q_0}{2 \alpha_e \beta_1} \left( 2 \exp[B_i^2 F_0 + \beta_1 (1 + u)] \text{erf}c \left( \frac{1 + u}{2 \sqrt{F_0}} + \beta_1 V_{F_0} \right) + \right. \]

\[ + \frac{2 \beta_1 V_{F_0}}{V \pi} \exp \left[ -\left( \frac{(1+u)^2}{4F_0} \right) \right] - (2 + \beta_1 + \beta_1 u) \text{erf}c \frac{1+u}{2 \sqrt{F_0}} \right) \],

\[ Q_2 = \frac{q_0}{\alpha_e \beta_1} \left[ \text{erf}c \left( \frac{u}{2 \sqrt{F_0}} \right) \right. - \left. \exp (\beta_1^2 F_0 + \beta_1 u) \text{erf}c \left( \frac{u}{2 \sqrt{F_0}} + \beta_1 V_{F_0} \right) \right], \]

\[ \text{ierf}c v = \frac{\exp(-v^2)}{V \pi} - v \text{erf}c v, \]

\[ \text{erf}c v = 1 - \text{erf} v = 1 - \frac{2}{V \pi} \int_0^v \exp(-v^2) dv. \]

The thermal power per unit surface area required for de-icing may be determined using the equation for \( t(b_1/6, F_0) \) at the time when the ice is shed. The temperature at the ice-blade interface varies with time according to the equation:

\[ t \left( \frac{b_1}{6}, F_0 \right) - t_0 = \frac{q_0}{\alpha_e} V_{F_0} \text{erf}c \left( \frac{k}{2 \sqrt{F_0}} \right) - \]

\[ - \frac{1}{\beta_1} \exp (\beta_1^2 F_0 + \beta_1 - \beta_1 k) \text{erf}c \left( \frac{2-k}{2 \sqrt{F_0}} + \beta_1 V_{F_0} \right) + \]

\[ + \frac{V_{F_0}}{V \pi} \exp \left[ -\left( \frac{(2-k)^2}{4F_0} \right) \right] - \frac{2 + 2 \beta_1 - \beta_1 k}{2 \beta_1} \text{erf}c \left( \frac{2-k}{2 \sqrt{F_0}} \right) \right) - \]

\[ - \frac{q_0}{\alpha_e \beta_1} \left[ \text{erf} \left( \frac{1-k}{2 \sqrt{F_0}} \right) \right. - \left. \exp (\beta_1^2 F_0 + \beta_1 - \beta_1 k) \times \right. \]

\[ \times \text{erf} \left( \frac{1-k}{2 \sqrt{F_0}} + \beta_1 V_{F_0} \right) \right]. \]

If the time at which the heater is switched on is given, we can obviously predetermine the heating power necessary for de-icing. At this power level the temperature at the ice-blade interface at the end of the on-time, \( F_{0on} \), must be equal to \( 0^\circ \text{C} \). Hence the required thermal power is determined from the equation

\[ q = \frac{q_0}{\beta_1} \left[ \text{erf} \left( \frac{1-k}{2 \sqrt{F_0}} \right) \right. - \left. \exp (\beta_1^2 F_0 + \beta_1 - \beta_1 k) \times \right. \]

\[ \times \text{erf} \left( \frac{1-k}{2 \sqrt{F_0}} + \beta_1 V_{F_0} \right) \right]. \]

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